Results of Proficiency Test Gasoil (premium) April 2021

Organized by: Institute for Interlaboratory Studies

Spijkenisse, the Netherlands

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Report: iis21G02 == revised ==

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SUMMARY OF CHANGES

This revised report replaces the original report iis21G02 of July 2021.

It was discovered that there was a copy error in the table of the parameter Distillation. The methods mentioned were of Density instead of Distillation.

This has no effect of the reported test results and the evaluation.

The following pages in this report has been revised:

- Appendix 1: page 24 and 27 (page 23 and 26 in the original report)

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1 Introduction

Over the past years, more and more diesel fuels are marketed with higher cetane numbers and additional cleaning agents and some synthetic content. These fuels are called premium diesel. The demand for these premium diesel fuels is increasing. Therefore, the Institute for Interlaboratory Studies (iis) decided to start with a proficiency test for Gasoil premium grade in 2020. During the annual proficiency testing program of 2020/2021 it was decided to continue the round robin for the analysis of Gasoil premium in accordance with EN590.

In this interlaboratory study registered for participation:

- 27 laboratories in 22 countries on Gasoil (premium)
- 14 laboratories in 11 countries for CN & DCN in Gasoil (premium)
- 14 laboratories in 14 countries for TC in Gasoil (premium)
- 14 laboratories in 14 countries for TC in Gasoil (premium)

In total 30 laboratories in 22 different countries registered for participation. See appendix 2 for the number of participants per country. In this report the results of this Gasoil (premium) proficiency tests are presented and discussed. This report is also electronically available through the iis website www.iisnl.com.

2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organizer of this proficiency test (PT). Sample analyzes for fit-for-use and homogeneity testing were subcontracted to an ISO/IEC17025 accredited laboratory. In this proficiency test the participants received, depending on the registration, from one to three different samples of premium Gasoil.

Sample	Quantity	Purpose
#21045	1 x 1L + 1x 0.5L	Regular analyzes
#21046	4 x 1L	Cetane Number & DCN
#21047	1 x 1L	Total Contamination

Table 1: samples used in Gasoil (premium) proficiency tests iis21G02

Participants were requested to report rounded and unrounded test results. The unrounded test results were preferably used for statistical evaluation.

2.1 ACCREDITATION

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, is accredited in agreement with ISO/IEC17043:2010 (R007), since January 2000, by the Dutch Accreditation Council (Raad voor Accreditatie). This PT falls under the accredited scope. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentiality of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on regular basis by sending out questionnaires.

2.2 PROTOCOL

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5). This protocol is electronically available through the iis website www.iisnl.com, from the FAQ page.

2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

2.4 SAMPLES

For the preparation of the sample for the regular PT of approximately 200 liters of premium Gasoil was obtained from the local market. After homogenisation 54 amber glass bottles of 1L and 54 amber glass bottles of 500 mL were filled and labelled #21045.

The homogeneity of the subsamples was checked by the determination of Density at 15°C in accordance with ISO12185 on 8 stratified randomly selected subsamples.

	Density at 15°C in kg/m³
sample #21045-1	835.33
sample #21045-2	835.33
sample #21045-3	835.30
sample #21045-4	835.33
sample #21045-5	835.30
sample #21045-6	835.32
sample #21045-7	835.31
sample #21045-8	835.31

Table 2: homogeneity test results of subsamples #21045

From the above test results the repeatability was calculated and compared with 0.3 times the reproducibility of the reference test method in agreement with the procedure of ISO13528, Annex B2 in the next table.

	Density at 15°C in kg/m³
r (observed)	0.04
reference test method	ISO12185:96
0.3 x R (reference test method)	0.15

Table 3: evaluation of the repeatability of subsamples #21045

The calculated repeatability was in agreement with 0.3 times the reproducibility of the reference test method. Therefore, homogeneity of the subsamples was assumed.

For the preparation of the sample for the PT on Cetane Number a batch of approximately 100 liters of Gasoil (premium) was obtained from the local market. After homogenization 90 amber glass bottles of 1L were filled and labelled #21046.

The homogeneity of the subsamples was checked by the determination of Density at 15°C in accordance with ISO12185 on 8 stratified randomly selected subsamples.

	Density at 15°C in kg/m³
sample #21046-1	835.33
sample #21046-2	835.32
sample #21046-3	835.33
sample #21046-4	835.33
sample #21046-5	835.33
sample #21046-6	835.32
sample #21046-7	835.33
sample #21046-8	835.33

Table 4: homogeneity test results of subsamples #21046

From the above test results the repeatability was calculated and compared with 0.3 times the reproducibility of the reference test method in agreement with the procedure of ISO13528, Annex B2 in the next table.

	Density at 15°C in kg/m³
r (observed)	0.01
reference test method	ISO12185:96
0.3 x R (reference test method)	0.15

Table 5: evaluation of the repeatability of subsamples #21046

The calculated repeatability was in agreement with 0.3 times the reproducibility of the reference test method. Therefore, homogeneity of the subsamples was assumed.

For the PT on Total Contamination the remaining amount of the same batch as used for the regular PT was selected. A defined volume of freshly prepared and well shaken dust suspension of Arizona Dust material in an oil was added to an 1L empty bottle by means of a calibrated pipette. The addition was checked by weighing the bottle before and after the addition. In total 30 bottles were prepared and subsequently filled up to 1L with premium Gasoil. Finally, the subsamples were labelled #21047.

Depending on the registration of the participant the appropriate set of PT samples was sent on March 17, 2021. An SDS was added to the sample package.

2.5 STABILITY OF THE SAMPLES

The stability of Gasoil packed in amber glass bottles was checked. The material was found sufficiently stable for the period of the proficiency test.

2.6 ANALYZES

The participants were requested to determine on sample #21045: Total Acid Number (TAN), Ash content, Calculated Cetane Index (four variables), Cloud Point, Cold Filter Plugging Point (CFPP), Carbon Residue (micro method) on 10% residue, Copper Corrosion 3hrs at 50°C, Density at 15°C, Distillation at 760 mmHg (IBP, 10%, 50%, 90%, 95% recovered, FBP and Volume at 250°C and 350°C), FAME, Flash Point PMcc, Kinematic Viscosity at 40°C, Lubricity by HFRR at 60°C, Manganese as Mn, Nitrogen, Polycyclic, Mono, Di, Tri+ and Total Aromatic Hydrocarbons, Pour Point (Manual and Automated), Sulfur and Water. On sample #21046 was requested to determine: Cetane Number and Derived Cetane Number (EN15195 and EN16715).

On sample #21047 was requested to determine: Total Contamination.

It was explicitly requested to treat the samples as if they were routine samples and to report the test results using the indicated units on the report form and not to round the test results but report as much significant figures as possible. It was also requested not to report 'less than' test results, which are above the detection limit, because such test results cannot be used for meaningful statistical evaluations.

To get comparable test results a detailed report form and a letter of instructions are prepared. On the report form the reporting units are given as well as the reference test methods (when applicable) that will be used during the evaluation. The detailed report form and the letter of instructions are both made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The participating laboratories are also requested to confirm the sample receipt on this data entry portal. The letter of instructions can also be downloaded from the iis website www.iisnl.com.

3 RESULTS

During five weeks after sample dispatch, the test results of the individual laboratories were gathered via the data entry portal www.kpmd.co.uk/sgs-iis/. The reported test results are tabulated per determination in appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline, a reminder was sent to those laboratories that had not reported test results at that moment. Shortly after the deadline, the available test results were screened for suspect data. A test result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the reported test results (no reanalyzes). Additional or corrected test results are used for data analysis and the original test results are placed under 'Remarks' in the test result tables in appendix 1. Test results that came in after the deadline were not taken into account in this screening for suspect data and thus these participants were not requested for checks.

3.1 STATISTICS

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5).

For the statistical evaluation the *unrounded* (when available) figures were used instead of the rounded test results. Test results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test, a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. If a data set does not have a normal distribution, the (results of the) statistical evaluation should be used with due care.

The assigned value is determined by consensus based on the test results of the group of participants after rejection of the statistical outliers and/or suspect data.

According to ISO13528 all (original received or corrected) results per determination were submitted to outlier tests. In the iis procedure for proficiency tests, outliers are detected prior to calculation of the mean, standard deviation and reproducibility. For small data sets, Dixon (up to 20 test results) or Grubbs (up to 40 test results) outlier tests can be used. For larger data sets (above 20 test results) Rosner's outlier test can be used. Outliers are marked by D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by F(0.01) for the Rosner's test. Stragglers are marked by F(0.01) for the Dixon's test, by F(0.01) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations.

For each assigned value the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement based on the target reproducibility in accordance with ISO13528. In this PT, the criterion of ISO13528, paragraph 9.2.1. was met for all evaluated tests, therefore, the uncertainty of all assigned values may be negligible and need not be included in the PT report.

Finally, the reproducibilities were calculated from the standard deviations by multiplying them with a factor of 2.8.

3.2 GRAPHICS

In order to visualize the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported test results are plotted. The corresponding laboratory numbers are on the X-axis. The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected reference test method. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle.

Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also, a normal Gauss curve (dotted line) was projected over the Kernel Density Graph (smooth line) for reference. The Gauss curve is calculated from the consensus value and the corresponding standard deviation.

3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. ISO, ASTM reproducibilities, the z-scores were calculated using a target standard deviation. This results in an evaluation independent of the variation in this interlaboratory study.

The target standard deviation was calculated from the literature reproducibility by division with 2.8. In case no literature reproducibility was available, other target values were used, like Horwitz or an estimated reproducibility based on former iis proficiency tests.

When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

The z-scores were calculated according to:

```
z_{\text{(target)}} = \text{(test result - average of PT)} / \text{target standard deviation}
```

The $z_{\text{(target)}}$ scores are listed in the result tables of appendix 1.

Absolute values for z<2 are very common and absolute values for z>3 are very rare. The usual interpretation of z-scores is as follows:

```
|z| < 1 good
1 < |z| < 2 satisfactory
2 < |z| < 3 questionable
3 < |z| unsatisfactory
```

4 **EVALUATION**

In this proficiency test some problems were encountered with the dispatch of the samples due to COVID-19 pandemic. Therefore, the reporting time on the data entry portal was extended with another week. For the regular premium Gasoil PT one participant did not report any test results at all and all participants report test results for the PT on Cetane Number in prepium Gasoil. For the PT on Total Contamination in premium Gasoil one participant did not report any test results at all.

In total 29 participants reported 553 numerical test results. Observed were 21 outlying test results, which is 3.8% of the numerical test results.

In proficiency studies, outlier percentages of 3%-7.5% are quite normal.

Not all original data sets proved to have a normal Gaussian distribution. These are referred to as "not OK" or "suspect". The statistical evaluation of these data sets should be used with due care.

4.1 EVALUATION PER SAMPLE AND PER TEST

In this section the reported test results are discussed per sample and per test. The test methods which were used by the various laboratories were taken into account for explaining the observed differences where possible and applicable. These test methods are also in the tables together with the original data. The abbreviations, used in these tables, are explained in appendix 3.

In the iis PT reports ASTM test methods are referred to with a number (e.g. D4737) and an added designation for the year that the test method was adopted or revised (e.g. D4737:10). If applicable, a designation in parentheses is added to designate the year of reapproval (e.g. D4737:10(2016)). In the results tables of appendix 1 only the test method number and year of adoption or revision e.g. D4737:10 will be used.

Sample #21045

<u>Total Acid Number</u>: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D974:14e2.

Ash content:

This determination may not be problematic. The consensus value was below the application range of ISO6245:01 and many participants reported a lower than test value. Therefore, no z-scores were calculated.

Calculated Cetane Index, four variables: Regretfully, no reproducibility is mentioned in procedure A of ASTM D4737:10(2016) nor in the equivalent test methods ISO4264 and IP380. Therefore, iis has estimated a reproducibility for Calculated Cetane Index by Four Variable Equation based from previous iis Gasoil PTs. This work done in 2019 has been reported in iis memo 1904 available on www.iisnl.com.

This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the reproducibility of iis memo 1904. No calculation errors were observed.

Cloud Point: This det

This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ISO3015:19.

CFPP: This determination was problematic. Two statistical outliers were observed.

The calculated reproducibility after rejection of the statistical outliers is not

in agreement with the requirements of EN116:15.

<u>Carbon Residue on 10% residue</u>: This determination was problematic. No statistical outliers were observed. However, the calculated reproducibility is not in agreement with the requirements of ISO10370:14.

<u>Copper Corrosion</u>: This determination was not problematic. All reporting laboratories agreed on a result of 1 (1a).

<u>Density at 15°C</u>: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ISO12185:96.

<u>Distillation</u>: This determination was problematic for the determination for Initial Boiling

Point. Most likely sample #21045 contained traces of light product. This affected the IBP and Flash Point PMcc. Therefore, it was decided to

calculate no z-scores for the Initial Boiling Point.

The determination was not problematic for all other Distillation parameters. Six statistical outliers were observed over eight parameters. All calculated reproducibilities (except IBP) after rejection of the statistical outliers are in agreement with the requirements of ISO3405:19 for automated mode as

well as for manual mode.

<u>FAME</u>: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of mode B of EN14078:14.

Flash Point PMcc: This determination was problematic. It appeared that the consensus value was below the application range of ISO2719A:16. Therefore, no z-scores were calculated. Most likely sample #21045 contained traces of light product. This had also affected the IBP in the Distillation Determination.

<u>Kinematic Viscosity at 40°C</u>: This determination was problematic. No statistical outliers were observed. The calculated reproducibility is not in agreement with the requirements of ISO3104:20.

<u>Lubricity</u>: This determination was not problematic. No statistical outliers were

observed. The calculated reproducibility is in agreement with the

requirements of modes A or B of ISO12156-1:18.

<u>Manganese</u>: This determination may not be problematic. The consensus value was

below the application range of EN16576:14. Therefore, no z-scores were

calculated.

<u>Nitrogen</u>: This determination was not problematic. Three statistical outliers were

observed. The calculated reproducibility after rejection of the statistical

outliers is in agreement with the requirements of ASTM D4629:17.

<u>Polycyclic Aromatic Hydrocarbons</u>: This determination was not problematic. No statistical outlies were observed. The calculated reproducibility is in agreement with

the requirements of EN12916:16.

- Mono Aromatic Hydrocarbons: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of EN12916:16.
- <u>Di Aromatic Hydrocarbons</u>: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of EN12916:16.
- <u>Tri+ Aromatic Hydrocarbons</u>: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of EN12916:16.
- <u>Total Aromatic Hydrocarbons</u>: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of EN12916:16.
- <u>Pour Point Manual</u>: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ISO3016:19.
- <u>Pour Point Automated</u>: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements ASTM D5950:14(2020)
- <u>Sulfur</u>: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ISO20846:19.
- <u>Water</u>: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ISO12937:00.

Sample #21046

- <u>Cetane Number</u>: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ISO5165:20.
- <u>DCN EN17155</u>: For DCN and Ignition Delay only one test result was reported, therefore no z-scores were calculated.
- <u>DCN EN16715</u>: This determination was problematic for Derived Cetane Number and Combustion Delay but not problematic for Ignition Delay. No statistical outliers were observed. The calculated reproducibilities of Derived Cetane Number and Combustion Delay are not in agreement with the requirements of EN16715:15. The calculated reproducibility of Ignition Delay is in agreement with the requirements of EN16715:15.

Sample #21047

<u>Total Contamination</u>: This determination was problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is not in agreement with the requirements of EN12662:14.

4.2 PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES

A comparison has been made between the reproducibility as declared by the reference test method and the reproducibility as found for the group of participating laboratories. The number of significant test results, the average, the calculated reproducibility (2.8 * standard deviation) and the target reproducibility derived from literature reference test methods (in casu ASTM, EN, ISO test methods) or previous proficiency tests are presented in the next tables.

Parameter	unit	n	average	2.8 * sd	R(lit)
Total Acid Number (TAN)	mg KOH/g	12	0.035	0.028	0.04
Ash content	%M/M	10	<0.001	n.e.	n.e.
Calc. Cetane Index four variables		23	53.19	0.70	0.91
Cloud Point	°C	20	-7.0	1.5	4
Cold Filter Plugging Point	°C	20	-25.3	5.4	4.5
Carbon Residue on 10% residue	%M/M	10	0.019	0.041	0.018
Copper Corrosion, 3hrs at 50°C		19	1 (1a)	n.a.	n.a.
Density at 15°C	kg/m³	24	835.4	0.3	0.5
Initial Boiling Point	°C	23	153.6	15.4	(8.5)
Temp at 10% recovery	°C	25	205.2	4.0	4.5
Temp at 50% recovery	°C	24	274.3	2.5	3.0
Temp at 90% recovery	°C	25	343.5	3.7	5.2
Temp at 95% recovery	°C	25	356.7	7.1	8.9
Final Boiling Point	°C	24	363.6	4.0	7.1
Volume at 250°C	%V/V	23	36.0	1.7	2.7
Volume at 350°C	%V/V	23	92.9	1.9	2.7
FAME	%V/V	14	6.77	0.37	0.50
Flash Point PMcc	°C	21	<40	n.e.	n.e.
Kinematic Viscosity at 40°C	mm²/s	20	2.811	0.051	0.031
Lubricity by HFRR	μm	14	182	49	80
Manganese as Mn	mg/L	7	<0.5	n.e.	n.e.
Nitrogen	mg/kg	8	20.2	2.2	3.8
Polycyclic Aromatic Hydrocarbons	%M/M	12	1.57	0.73	0.76
Mono Aromatic Hydrocarbons	%M/M	10	15.3	1.5	1.9
Di Aromatic Hydrocarbons	%M/M	10	1.48	0.40	0.45
Tri ⁺ Aromatic Hydrocarbons	%M/M	11	0.09	0.11	0.51
Total Aromatic Hydrocarbons	%M/M	10	16.9	1.7	1.8
Pour Point Manual	°C	17	-32.1	4.9	9
Pour Point Automated	°C	8	-31.1	4.4	6.1

Parameter	unit	n	average	2.8 * sd	R(lit)
Sulfur	mg/kg	23	7.5	1.9	2.0
Water	mg/kg	20	55.3	29.9	51.1

Table 6: reproducibilities of tests on sample #21045

Parameter	unit	n	average	2.8 * sd	R(lit)
Cetane Number		9	52.6	1.8	4.4
DCN (EN17155)		1	n.e.	n.e.	n.e.
Ignition Delay (EN17155)	ms	1	n.e.	n.e.	n.e.
DCN (EN16715)		5	53.4	2.6	1.5
Ignition Delay (EN16715)	ms	5	3.0	0.08	0.16
Combustion Delay (EN16715)	ms	5	4.5	0.19	0.13
Total Contamination	mg/kg	12	19.5	13.4	7.5

Table 7: reproducibilities of tests on samples #21046 and #21047

Without further statistical calculations it can be concluded that for several tests there is a good compliance of the group of participating laboratories with the reference test methods. The problematic tests have been discussed in paragraph 4.1.

4.3 COMPARISON OF THE PROFICIENCY TEST OF APRIL 2021 WITH PREVIOUS PT

	April 2021	April 2020
Number of reporting laboratories	29	30
Number of test results	553	618
Number of statistical outliers	21	15
Percentage of statistical outliers	3.8%	2.4%

Table 8: comparison with previous proficiency test

In proficiency tests, outlier percentages of 3% - 7.5% are guite normal.

The performance of the determinations of this proficiency test was compared against the requirements of the reference test methods. The conclusions are given the following table.

Parameter	April 2021	April 2020
Total Acid Number (TAN)	+	+
Ash content	n.e.	++
Calc. Cetane Index four variables	+	+
Cloud Point	++	+
Cold Filter Plugging Point	-	-
Carbon Residue on 10% residue		+/-
Density at 15°C	++	++
Distillation at 760 mmHg	-	+
FAME	+	+/-

Parameter	April 2021	April 2020
Flash Point PMcc	n.e.	+
Kinematic Viscosity at 40°C	-	+/-
Lubricity by HFRR	+	+
Manganese as Mn	n.e.	n.e.
Nitrogen	+	-
Polycyclic Aromatic Hydrocarbons	+/-	+
Mono, Di and Tri ⁺ Aromatic HCs	+	+
Total Aromatic Hydrocarbons	+	++
Pour Point	+	+
Sulfur	+/-	+
Water	+	++
Cetane Number	+	+
DCN (EN17155)	n.e.	-
DCN (EN16715)	-	-

Table 9: comparison determinations against the reference test method

The following performance categories were used:

++ : group performed much better than the reference test method

+ : group performed better than the s reference test method

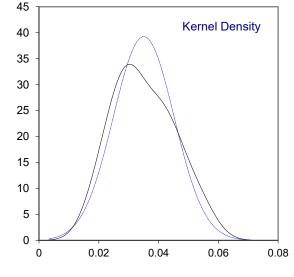
+/- : group performance similar to the reference test method

- : group performed worse than the reference test method

-- : group performed much worse than the reference test method

n.e. : not evaluated

lab	mination method		value				marks	,				
171 192	D974		0.04			0.35						
196	D974		0.0275			-0.53						
541	D974		<0.05									
324	D974		0.03			-0.35						
962 963	D974		0.02			 -1.05						
121	D664-A		0.02			0.63						
26	200.7.											
41												
259	D664-A		0.023			-0.84						
320 556	D664-A		0.054			1.33						
20	D004-A D974		0.034			-0.35						
'53	20, 1											
76	D664-A		<0.1									
06												
54 57	D664-A		0.03			-0.35						
57 80	D974		0.047			0.84						
18												
28												
75												
01	D664-A		0.04			0.35						
74 666	D974		0.035			0.00						
78	D374											
	normality		OK									
	n		12									
	outliers mean (n)		0 0.0350	1								
	st.dev. (n)		0.0330									
	R(calc.)		0.0284									
	st.dev.(D9		0.0142	86								
	R(D974:14	∔e2)	0.04									
0.1 T												
.08 +												
0.06												Δ
0.04								Δ	Δ	Δ	Δ	
			Δ	Δ	Δ	Δ	Δ					,
	Δ	Δ										
0.02												
0.02					_	24	998	171	6201	121	1857	ω.
0 -		1259	496	824	1720	1854	8		29	=	~	1556
0 -	693	1259	96	824	17.20	38	8		8	<u> </u>		155
0.02 -	683	1259		Kernel [8		<u> </u>	159



Determination of Ash content on sample #21045; result in %M/M

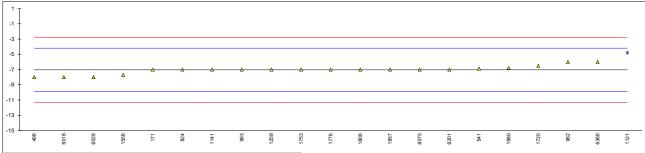
lab	method	value	mark	z(targ)	remarks
171	D482	<0.010			
492					
496					
541	ISO6245	<0.001			
824	ISO6245	<0.01			
962	D482	0.0003			
963	ISO6245	<0.001			
1121	ISO6245	0.00048			
1126					
1141					
1259					
1320					
1556	ISO6245	0.0004			
1720					
1753	ISO6245	0.0006			
1776					
1806					
1854	ISO6245	0.0009			
1857	ISO6245	0.0029			
1980	ISO6245	0.0013			
6018					
6028					
6075	ISO6245	<0.001			
6201	ISO6245	0.0012			
6274	ISO6245	<0.001			
6366	D482	< 0.001			
6378					
		40			
	n 	10			
	mean (n)	<0.001			

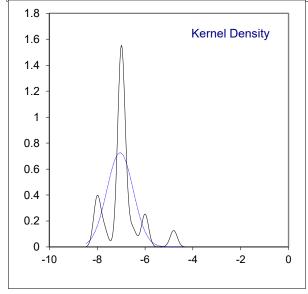
Determination of Calculated Cetane Index, four variables on sample #21045

lab	method			valu		mar	k	z(taı		remai	ks									
171	D4737-A	-		53.1				-0.												
492 496	ISO4264			53.2					03											
541	D4737-A			53.4					86											
824				53.2					03											
962	D4737-A			53.3					34											
963	ISO4264			53.6					26											
1121 1126	ISO4264			52.8				-1.	05 											
1141	ISO4264			53.0				-0.												
1259	ISO4264			53.1				- 0.												
1320																				
1556	ISO4264			53.2					03											
1720 1753	D4737-A ISO4264			53.4 52.9				0. - 0.	65 62											
1776	ISO4264			53.0				-0. -0.												
1806	ISO4264			52.8	38			- 0.												
1854	D4737-A			53.0				-0.												
1857	ISO4264			53.8					88											
1980 6018	ISO4264 ISO4264			53.3 53.6		С			34 26	first re	norte	1 53 9								
6028	ISO4264			53.2	2	O			03	1113110	porte	1 00.0								
6075	ISO4264			53.1	15			-0.	13											
6201	ISO4264			53.1				-0.												
6274	ISO4264			53.1				- 0.												
6366 6378	D4737-A			52.8	55			-1. 												
0010																				
	normality			OK																
	n			23																
	outliers mean (n)			0 53.1	101															
	st.dev. (n))		0.24																
	R(calc.)			0.69	97															
	st.dev.(iis	memo	1904)																	
	R(iis mem	10 1904	4)	0.90) (
54.5 T																				
54 -																				
53.5 -														Δ	Δ	Δ	Δ	Δ	Δ	
53 + A	Δ Δ	Δ	Δ	Δ	Δ	Δ	Δ	Δ	-											
52.5 - 52 -																				
51.5																				
51 -																				
50.5																				
50	986	1753	141	1776	1854	171	6201	6274	9075	496	824	1556	8028	962	1980	1720	142	963	8018	1857
= =====================================	63	17		14	8	- 2	8		.09	4	80	12	8	6	19	12	ı,	6	8	89
2							_													
					(orno	l Density	,													
1.8	1		\wedge	-	(enie	Density														
1.6	1			k.																
			- [/	//																
1.4	-																			
1.2																				
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0.0			//																	
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0.4	1	/			//															
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	1 .	//			/															
0	+							_												
	52 52.	5	53	53.	.5	54	54.5	P												

Determination of Cloud Point on sample #21045; result in °C

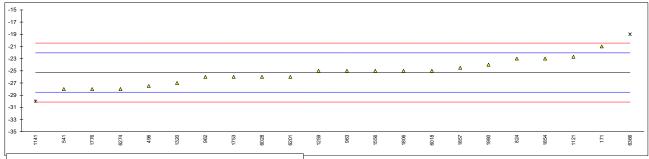
lab	method	value	mark	z(targ)	remarks
171	D2500	-7		0.03	
492					
496	ISO22995	-8		-0.67	
541	D5771	-6.9		0.10	
824	ISO3015	-7		0.03	
962	D2500	-6		0.73	
963	ISO3015	-7		0.03	
1121	ISO3015	-4.8	G(0.05)	1.57	
1126			,		
1141	ISO3015	-7		0.03	
1259	EN23015	-7		0.03	
1320					
1556	ISO3015	-7.7		-0.46	
1720	D5773	-6.5		0.38	
1753	ISO3015	-7		0.03	
1776	ISO3015	-7		0.03	
1806	D2500	-7		0.03	
1854	D2000	, 			
1857	ISO3015	-7		0.03	
1980	ISO3015	-6.8		0.03	
6018	ISO3015	-8		-0.67	
6028	D2500	-8		-0.67	
6075	EN23015	-0 -7		0.03	
6201	ISO3015	-7 -7		0.03	
6274	1000010				
6366	D2500	-6		0.73	
6378	D2500				
0010					
	normality	OK			
	n	20			
	outliers	1			
	mean (n)	-7.04			
	st.dev. (n)	0.550			
	R(calc.)	1.54			
	st.dev.(ISO3015:19)	1.429			
	R(ISO3015:19)	4			
	compare	-			
	R(ISO22995:19)	2.5			
	11(10022333.13)	2.0			
1 _T					
-1 +					
-3 + _					
-5 +					<u>.</u>

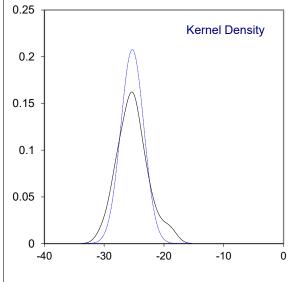




Determination of Cold Filter Plugging Point (CFPP) on sample #21045; result in °C

D6371 EN116 EN116 EN116 D6371 EN116 IP309	-21 -27.5 -28 -23 -26		2.66 -1.37 -1.68	
EN116 EN116 D6371 EN116	-27.5 -28 -23 -26		-1.37 -1.68	
EN116 EN116 D6371 EN116	-28 -23 -26		-1.68	
EN116 D6371 EN116	-23 -26			
D6371 EN116	-26		4 40	
EN116			1.42	
	~-		-0.44	
IP309	-25		0.18	
	-22.7		1.60	
EN116	-30	G(0.05)		
EN116	-25			
EN116	-27		-1.06	
EN116	-25		0.18	
EN116				
EN116				
EN116			-0.44	
D6371	-19	G(0.05)	3.90	
normality	OK			
n	20			
outliers				
mean (n)	-25.29			
st.dev. (n)				
R(calc.)				
st.dev.(EN116:15)	1.613			
R(EN116:15)	4.52			
	EN116 D6371	EN116 -25 EN116 -27 EN116 -25 EN116 -25 EN116 -26 EN116 -28 EN116 -25 EN116 -23 EN116 -24.5 EN116 -24.0 EN116 -25 EN116 -25 EN116 -26 EN116 -28 D6371 -19 normality OK n 20 outliers 2 mean (n) -25.29 st.dev. (n) 1.922 R(calc.) 5.38 st.dev.(EN116:15) 1.613	EN116 -25 EN116 -27 EN116 -25 EN116 -25 EN116 -26 EN116 -28 EN116 -25 EN116 -23 EN116 -24.5 EN116 -24.0 EN116 -25 EN116 -26 EN116 -26 EN116 -26 EN116 -26 EN116 -26 EN116 -26 EN116 -28 D6371 -19 G(0.05) normality OK n 20 outliers 2 mean (n) -25.29 st.dev. (n) 1.922 R(calc.) 5.38 st.dev.(EN116:15) 1.613	EN116





Determination of Carbon Residue (Micro method) on 10% residue on sample #21045; result in %M/M

lab	method	value	mark	z(targ)	remarks				
171									
492									
496	ISO10370	0.026		1.02					
541	ISO10370	<0.10		4.00					
824 962	ISO10370 D4530	0.030 0.0060		1.63 -2.01					
963	ISO10370	<0.1		-2.01					
1121	ISO10370	0.048		4.35					
1126									
1141									
1259									
1320	10040070	0.0045		2.00					
1556 1720	ISO10370	0.0015		-2.69					
1753									
1776									
1806									
1854	ISO10370	0.03		1.63					
1857	ISO10370	0.006		-2.01					
1980 6018	ISO10370	0.007		-1.85 					
6028	ISO10370	0.02		0.11					
6075	ISO10370	0.018		-0.19					
6201	ISO10370	<0,10							
6274	ISO10370	<0.1							
6366	D4530	<0.10							
6378									
	normality	OK							
	n	10							
	outliers	0							
	mean (n)	0.01925							
	st.dev. (n)	0.014612							
	R(calc.)	0.04091 0.006604							
	st.dev.(ISO10370:14) R(ISO10370:14)	0.008604							
0.06									
0.05									Δ
0.04 -									
0.03 +							Δ	Δ	
0.02 +					•	Δ			
				Δ					
0.01		Δ	Δ						
0 +	Δ								
-0.01	962	1857	1980	9075	9028	4 96	824	1854	1121
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		Kerner	Density						
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	.05 0	0.05		0.1					
				U.I I					
-0	.00	0.00	,	0.1					

Determination of Copper Corrosion, 3hrs at 50°C on sample #21045

lab	method	value	mark	z(targ)	remarks
171					
492					
496					
541	D130	1a			
824	D130	1a			
962	D130	1A			
963	D130	1a			
1121	IP154	1a			
1126					
1141	ISO2160	class 1			
1259					
1320	D130	1a			
1556	ISO2160	class 1			
1720	D130	1a			
1753	ISO2160	1a			
1776					
1806					
1854	D130	1A			
1857	D130	1a			
1980	ISO2160	1			
6018	ISO2160	1a			
6028	ISO2160	1a			
6075	ISO2160	1a			
6201	D130	1a			
6274	D130	1A			
6366	D130	1A			
6378					
	n	19			
	mean (n)	1 (1a)			
		. (14)			

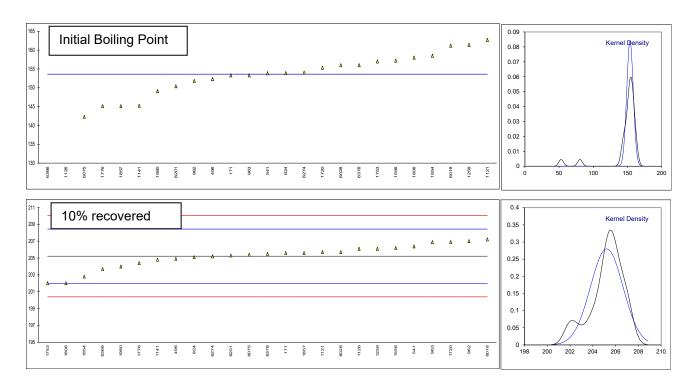
Determination of Density at 15°C on sample #21045; result in kg/m³

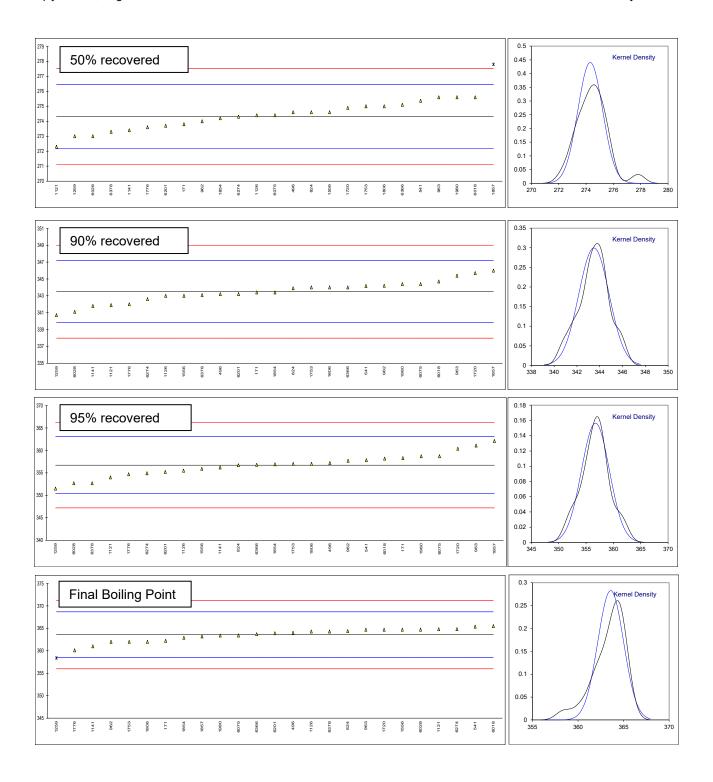
lab	method				lue		ma	ark		z(targ		remai	rks										
171	D4052				35.4					0.05													
492	D 4050																						
496 541	D4052 ISO1218	0.5			35.26 35.35					-0.73 -0.23													
824	ISO121				35.4					0.05													
962	D4052	50			35.3					-0.51	ĺ												
963	ISO121	85			35.3					-0.51													
1121	ISO1218				35.4					0.05													
1126	ISO1218				35.35					-0.23													
1141	ISO121				35.4					0.05													
1259	ISO121	85			35.3					-0.51													
1320	100404	0.5								4.00													
1556 1720	ISO1218 D4052	85			35.58 35.375	5				1.06 -0.09													
1753	ISO1218	85			35.57 S	,				0.61													
1776	ISO121				35.4					0.05													
1806	ISO367				35.6					1.17													
1854	ISO1218				35.35					-0.23													
1857	ISO1218				35.4					0.05													
1980	ISO121				35.45					0.33													
6018	ISO1218				35.3					-0.51													
6028 6075	ISO1218				35.2 35.49					-1.07 0.55													
6201	D4052	55			35.49					0.33													
6274	ISO1218	85			35.5					0.61													
6366	D4052	50			35.35					-0.23	3												
6378	D1298				34.7		C,l	R(0.0	1)	-3.87		first re	porte	d 836	3								
								`	,				•										
	normalit	У		Ol																			
	n			24	ļ																		
	outliers	,		1																			
	mean (n				35.39	1																	
	st.dev. (R(calc.)				0961 269																		
	st.dev.(I		85.96)		1786																		
	R(ISO12	2185:96	S) (0.	5																		
000 5																							
836.5 T																							
836.5 T																							
																		Δ	Δ	Δ	Δ	Δ	
836	Δ 4	Δ Δ	Δ	Δ	Δ	Δ	Δ	Δ	Δ	Δ								Δ	Δ	Δ	Δ	Δ	
836	Δ 4	Δ Δ	Δ	Δ		Δ	Δ	Δ	Δ	Δ		Δ		Δ	Δ	Δ_	٨	Δ	Δ	Δ	Δ	Δ	
836 835.5 835 *	Δ	Δ Δ	Δ	Δ		Δ	Δ	Δ	Δ	Δ	Δ.	Δ				Δ	A	Δ	Δ	Δ	Δ	Δ	Δ
836 835.5	Δ	Δ Δ	Δ	Δ		Δ	Δ	Δ	Δ	Δ		Δ	۵	Δ	Δ	Δ		Δ	Δ	Δ	Δ	Δ	Δ
836 835.5 835 834.5 -	*				Δ	Δ	Δ	Δ	Δ	Δ	Δ.	Δ	۵	<u> </u>	Δ	Δ	^	Δ					
836 835.5 835 *	:	∆ △	Δ	▲ 286		δ41	1128 A	Δ	63.66	7280	431	4121	854	1141	1776	1857	6201	1990	△	4753	6274	15.08	1806
836	*				Δ	P 641	4128	1854	9889	4720	421	1121	824	1141	97.11	1857	0201	△ 0861					
836 835.5 835 834.5 -	*				Δ	541	4128	₫	9968	43.20	121	1121	824	1141	17.76	1857	1029	△					
836	*				Ø108				9869	1720	4	1121	4 878 878 878 878 878 878 878 878 878 87	1141	1776	1857	62201	0861					
836	*				Ø108		& Ben		8866	428	421	1121	824	1141	97.17	1867	1029						
835.5 835.5 * * * * * * * * * * * * * * * * *	*				Ø108				8869	77.20	121	1121	A 100 100 100 100 100 100 100 100 100 10	1141	1776	Z381	1029	Q9 61					
836	*				Ø108				99.55	0271	121	1121	N7.8	1141	4777	1857	11028	△					
835.5 835.5 * * * * * * * * * * * * * * * * *	*				Ø108				A 9955	QZ L1	4	1121	N. 28	1141	3777	1857	1029	△					
835.5 835.5 * * * * * * * * * * * * * * * * *	*				Ø108				9969	A 02.21		4121	824	1141	3777	2827	1029	△					
835.5	*				Ø108				9969	42.27	141	1121	824	1141	87.77	2587	1029	△					
835.5 835.5 * * * * * * * * * * * * * * * * *	*				Ø108				898	47.20	141	1211	824	1141	87.77	2582	1029	△					
835.5 + * * * 834.5 + - * * * * * * * * * * * * * * * * * *	*				Ø108				998	42.00	4	1211	₽	1141	8777	1827	1020	A 1966.					
835.5	*				Ø108				9969	420	121	1211	₽	1141	8777	1827	1020	A 10864					
835.5 * 835.5 * 834.5 - * 4.5 - 4 3.5 - 3 2.5 - 2	*				Ø108				9969	4.00	42	1211	824	1141	8777	1827	1029	D864					
835.5 + * * * 834.5 + - * * * * * * * * * * * * * * * * * *	*				Ø108				9900	4.20	121	1211	824	1141	8777	1827	1029	△					
835.5 4.5 4.5 4.5 3.5 3 2.5 2	*				Ø108				9963	4.20	11 L	1211	4728	1141	8777	4 1827	1029	A 0865					
835.5 * 835.5 * 834.5 - * 4.5 - 4 3.5 - 3 2.5 - 2	*				Ø108				9900	4.20	4	1211	824	1141	87.77	4 2581	1029	△					
835.5 4.5 4.5 4.5 3.5 2.5 2	*				Ø108				99639	4.20	4	1211	478	1141	87.77	2581	1029	A 0864					
835.5 4.5 4.5 4.5 3.5 3 2.5 2	*				Ø108				99639	A 02.21	4	1121	478	1141	87.77	4 2581	1029	A 0864					
835.5 4 834.5 4 3.5 3 2.5 2 1.5 1 0.5 0	8200				Ø108				9963	4120	4	1121	728	1141	87.77	4 2581	11000	A 0865					
835.5 4 834.5 4 3.5 3 2.5 2 1.5 1 0.5 0	*				Δ Ke	ernel		sity	836	4120	4 141	1121	A 1728	1141	9221	4 2581	11029	0865					
835.5 4 834.5 4 3.5 3 2.5 2 1.5 1 0.5 0	8200	8627.		226	Δ Ke	ernel	Den	sity		0221	Ε.	1121 A	A 1828	1141	9221	4 2581	1000	△					

Determination of Distillation at 760 mmHg on sample #21045; result in °C

lab	method	IBP	10%rec	50%rec	90%rec	95%rec	FBP
171	D86-automated	153.3	205.6	273.8	343.4	358.3	362.2
492							
496	D86-automated	152.3	204.9	274.6	343.2	357.2	364.0
541	D86-automated	153.84	206.38	275.37	344.17	357.86	365.39
824	ISO3405-automated	153.9	205.1	274.6	343.9	356.7	364.4
962	D86-automated	151.8	207.0	274.0	344.2	357.7	362.0
963	ISO3405-automated	153.3	206.9	275.6	345.4	361.1	364.7
1121	ISO3405-automated	162.7	205.7	272.3	341.9	354.0	364.8
1126	ISO3405-automated	80.7 R(1)	206.1	274.4	343.0	355.5	364.3
1141	ISO3405-automated	145.2	204.8	273.4	341.8	356.2	361.0
1259	D86-automated	161.4	206.1	273.0	340.7	351.5	358.4 R(5)
1320							
1556	ISO3405-automated	157.2	206.2	274.6	343.0	355.9	364.7
1720	D86-automated	155.3	206.9	274.9	345.7	360.4	364.7
1753	ISO3405-manual	157	202	275	344	357	362
1776	ISO3405-automated	145.1	204.4	273.6	342.0	354.7	360.1
1806	ISO3405-manual	158	202	275	344	357	362
1854	D86-automated	158.5	202.8	274.2	343.4	356.9	362.9
1857	ISO3405-automated	145.1	205.6	277.8 R(5)	346	362.1	363.2
1980	ISO3405-automated	149.1	204.0	275.6	344.4	358.7	363.4
6018	ISO3405-automated	161.2	207.2	275.6	344.7	358.2	365.5
6028	ISO3405-automated	156.0	205.7	273.0	341.1	352.7	364.7
6075	ISO3405-automated	142.3	205.4	274.4	344.4	358.7	363.4
6201	D86-automated	150.4	205.3	273.7	343.2	355.2	363.9
6274	D86-automated	154	205.2	274.3	342.6	354.9	364.8
6366	D86-automated	53.0 R(1)	203.7	275.1	344.0	356.8	363.7
6378	D86-manual	156.0	205.5 C	273.3 C	343.1 C	352.7 C	364.3 C
	normality	ОК	ОК	ОК	ОК	ОК	ок
	n	23	25	24	25	25	24
	outliers	2	0	1	0	0	1
	mean (n)	153.61	205.22	274.31	343.49	356.72	363.59
	st.dev. (n)	5.487	1.426	0.906	1.332	2.549	1.411
	R(calc.)	15.36	3.99	2.54	3.73	7.14	3.95
	st.dev.(ISO3405-A:19)	(3.017)	1.612	1.071	1.840	3.177	2.536
	R(ISO3405-A:19)	(8.45)	4.51	3.00	5.15	8.90	7.10
	compare						
	R(ISO3405-M:19)	(7.60)	5.01	4.10	4.24	4.47	3.68
	14(1000-100 M.10)	(1.00)	1 0.01	1 -1.10	T. 2 T	1	1 0.00

Lab 6378 first reported 153.0; 208.8; 281.6; 355.4; 368.1; 376.5 respectively





z-scores Distillation on sample #21045

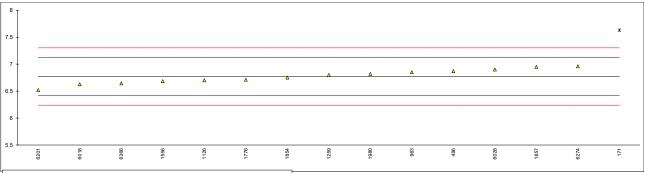
lab	IBP	10%rec	50%rec	90%rec	95%rec	FBP
171		0.24	-0.47	-0.05	0.50	-0.55
492						
496		-0.20	0.27	-0.16	0.15	0.16
541		0.72	0.99	0.37	0.36	0.71
824		-0.07	0.27	0.22	-0.01	0.32
962		1.10	-0.29	0.39	0.31	-0.63
963		1.04	1.21	1.04	1.38	0.44
1121		0.30	-1.87	-0.86	-0.86	0.48
1126		0.55	0.09	-0.27	-0.38	0.28
1141		-0.26	-0.85	-0.92	-0.16	-1.02
1259		0.55	-1.22	-1.52	-1.64	-2.05
1320						
1556		0.61	0.27	-0.27	-0.26	0.44
1720		1.04	0.55	1.20	1.16	0.44
1753		- 2.00	0.65	0.28	0.09	-0.63
1776		-0.51	-0.66	-0.81	-0.64	-1.38
1806		-2.00	0.65	0.28	0.09	-0.63
1854		-1.50	-0.10	-0.05	0.06	-0.27
1857		0.24	3.26	1.36	1.69	-0.15
1980		-0.76	1.21	0.49	0.62	-0.07
6018		1.23	1.21	0.66	0.47	0.75
6028		0.30	-1.22	-1.30	-1.26	0.44
6075		0.11	0.09	0.49	0.62	-0.07
6201		0.05	-0.57	-0.16	-0.48	0.12
6274		-0.01	-0.01	-0.48	-0.57	0.48
6366		-0.94	0.74	0.28	0.03	0.04
6378		0.17	-0.94	-0.21	-1.26	0.28

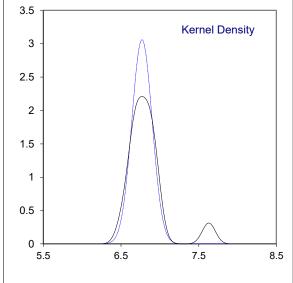
Determination of Distillation on sample #21045; result in %V/V

171	lab	method	Vol.250°C	mark	z(targ)	Vol.350°C	mark	=	z(targ)	remarks
## 1		metriou	ī	mark			mark			Temarks
541 D86-automated 36.8										
824 ISC3405-automated 962 D86-automated 36.3 0.30 92.7 0.16 992 D86-automated 963 ISC3405-automated 37.3 1.34 93.6 0.78 1121 ISC3405-automated 37.3 1.34 93.6 0.78 1121 ISC3405-automated 37.3 1.34 93.6 0.78 1121 ISC3405-automated 35.9 0.12 93.2 0.36 1141 ISC3405-automated 35.9 0.12 93.2 0.36 1141 ISC3405-automated 36.1 0.99 94.4 1.66 112 0.99 94.4 1.66 1	496	D86-automated								
982 D86-automated 36.4										
983 S03405-automated 35.8 -0.22 91.9 -0.99										
1128 ISO3405-automated 35.3 1.34 93.6 0.78 1.26 ISO3405-automated 35.3 0.74 93.2 0.36 1.26 ISO3405-automated 36.1 0.09 94.4 1.60 0.26 1.25 0.26 0.26 1.25 0.26 0.26 1.25 0.26 0.26 1.25 0.26 0.26 1.25 0.26 0.26 1.25 0.25										
1126 SG3405-automated 35.3 -0.74 93.2 0.36 1299 D86-automated 35.9 -0.12 93.2 0.36 1299 D86-automated 36.1 0.09 94.4 1.60 1.6										
1141 ISO3405-automated 36.1										
1329 D86-automated 36.1 0.09 94.4 1.60 1320										
1320 1556 ISO3405-automated 36.2 0.19 93.1 0.26 1720 D86-automated 36.4 0.40 91.9 -0.99 1753 ISO3405-manual 35 -1.05 93 0.15 176 ISO3405-automated 36.7 0.71 93.5 0.67 1806 ISO3405-automated 36.4 0.40 92.6 -0.26 1857 ISO3405-automated 36.4 0.40 92.6 -0.26 1857 ISO3405-automated 35.7 -0.32 92.4 -0.47 1806 ISO3405-automated 35.7 -0.32 92.4 -0.47 1806 ISO3405-automated 35.7 -0.32 92.4 -0.57 1806 ISO3405-automated 37.1 1.13 94.1 1.29 92.3 -0.57 1806 ISO3405-automated 37.1 1.13 94.1 1.29 1807 ISO3405-automated 36.4 0.40 93.2 0.36 1807 ISO3405-automated 36.4 0.40 93.2 0.36 1806 ISO3405-automated 36.4 0.40 93.2 0.36 ISO3405-automated 36.4 0.40 93.2 0.40 ISO3405-automated 36.4 0.40 ISO3405-automated 36.4 0.40										
1720										
1753 ISO3405-manual 35	1556	ISO3405-automated	36.2		0.19	93.1			0.26	
1776 ISOS405-automated 36.7 0.71 93.5 0.67 1806 ISOS405-manual 35 1.05 93 0.15 1854 D86-automated 36.4 0.40 92.6 0.26 1.20 1857 ISOS405-automated 35.7 0.32 92.4 0.47 0.57 0.6018 ISOS405-automated 35.7 0.32 92.4 0.47 0.57 0.6028 ISOS405-automated 35.7 0.32 92.3 0.57 0.57 0.57 0.50 0.57 0.50 0.57 0.50										
1806 ISO3405-manual 35										
1854 D86-automated 36.4 0.40 92.6 -0.26 1857 ISOS/405-automated 35.7 -0.32 92.4 -0.47 1808 ISOS/405-automated 35.7 -0.32 92.4 -0.47 1808 ISOS/405-automated 35.7 -0.32 92.4 -0.47 1808 1805/405-automated 36.1 -0.31 94.1 1.29 1.29 1.20										
1857 ISO3405-automated 35										
1980 ISO3405-automated 35.7										
6018 ISO3405-automated 35.7										
6028 ISO3405-automated 37.1 1.13 94.1 1.29 675 ISO3405-automated 36.3 0.30 92.3 -0.57 6201 D86-automated 36.4 0.40 93.2 0.36 6274 D86-automated 36.1 0.09 93.3 0.46 D86-automated 35.4 0.84 92.7 0.16 0.636 D86-automated 35.4 0.84 92.7 0.16 0.636 D86-automated 35.4 0.84 92.7 0.16 0.6378 D86-manual 39.5 C,R(0.01) 3.62 96.0 C,R(0.01) 3.26 fr. 37.5; 90.5 0.00 0.00 0.00 0.00 0.00 0.00 0.00										
6075 ISO3405-automated 36.3 0.30 92.3 -0.57 6201 D86-automated 35.4 0.40 93.2 0.36 6274 D86-automated 35.1 0.09 93.3 0.46 6366 D86-automated 35.4 0.64 92.7 0.16 6378 D86-manual 39.5 C,R(0.01) 3.62 96.0 C,R(0.01) 3.26 fr. 37.5; 90.5 normality OK n 23 0.23 0.046 92.7 0.16 92.85 0.00 Utiliers 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1										
6201 D86-automated 36.4 0.40 93.2 0.36 6274 D86-automated 35.1 0.09 93.3 0.46 6368 D86-automated 35.4 0.64 92.7 -0.16 35.4 0.64 92.7 -0.16 6378 D86-manual 39.5 C,R(0.01) 3.62 96.0 C,R(0.01) 3.26 fr. 37.5; 90.5 normality OK n										
6274 D86-automated 36.1 0.09 93.3 0.46 6366 D86-automated 35.4 0.09 93.3 0.46 6378 D86-manual 39.5 C,R(0.01) 3.62 96.0 C,R(0.01) 3.26 ff. 37.5; 90.5 normality OK										
6366 D86-automated 39.5 C,R(0.01) 3.62 92.7										
normality OK n 23										
n 23 outliers 1 1 1 92.85 st.dev. (n) 0.620	6378	D86-manual	39.5	C,R(0.01)	3.62	96.0	C,R(0	0.01)	3.26	fr. 37.5; 90.5
n 23 outliers 1 1 1 92.85 st.dev. (n) 0.620		normality	OK			OK				
outliers mean (n) 36.01 92.85 st.dev. (n) 0.620 0.686 R(calc.) 1.74 1.92 st.dev. (ISO3405-A:19) 2.7 2.7 compare R(ISO3405-M:19) 2.53 2.17 Volume at 250°C The street of the street										
mean (n) 36.01 st.dev. (n) 0.620 R(calc.) 1.74 1.92 st.dev. (ISO3405-A:19) 0.964 R(ISO3405-A:19) 2.7 compare R(ISO3405-A:19) 2.53 2.17										
st.dev.(n) 0.620 R(calc.) 1.74 st.dev.(lSO3405-A:19) 0.964 R(ISO3405-A:19) 2.7 compare R(ISO3405-M:19) 2.53 Volume at 250°C Volume at 350°C Volume at 350°C Kernel Density Volume at 350°C Kernel Density Kernel Density Kernel Density Kernel Density										
R(calc.) 1.74 st.dev.(ISO3405-A:19) 0.964 R(ISO3405-A:19) 2.7 compare R(ISO3405-M:19) 2.53 Volume at 250°C Volume at 250°C Volume at 350°C Volume at 350°C Kernel Density Volume at 350°C Kernel Density										
R(ISO3405-A:19) 2.7 2.17 Volume at 250°C						1.92				
Compare R(ISO3405-M:19) 2.53 2.17 Volume at 250°C										
R(ISO3405-M:19) 2.53 2.17			2.7			2.7				
Volume at 250°C x 0.7 0.6 0.5 0.7 0.6 0.7 0.7 0.7 0.7 0.7 0.7			0.50			0.47				
Volume at 250°C Volume at 250°C		K(1503405-W. 19)	2.53			2.17				
Volume at 250°C Volume at 250°C										
38	1 Val	ume at 250°C	1				x	0.7	-0	Kernel Density
To a second seco	39	unie at 250 C						0.6 -	M	Remer Density
Volume at 350°C X	38							0.5 -	// \	
Volume at 350°C	37					Δ	^		// \	
33	36 -	Δ	Δ Δ Δ	_ Δ Δ Δ	Δ Δ Δ	Δ		0.4	// \	
0.1 0.1 0.2 34 36 38 40 42 Volume at 350°C	35 + Δ Δ							0.3 -	/	
0.1 0.1 0.2 34 36 38 40 42 Volume at 350°C								0.2 -	// \	
32									// \	
97 Volume at 350°C x A A A A A A A A A A A A	33 +							0.1 -	/	
97 Volume at 350°C x 0.6 0.5 0.4 0.3 0.2 0.1 0.2 0.1		24 86 12 85	141	22 25 25 27 27 27 27 27 27 27 27 27 27 27 27 27	2 2 2 88 2 2 2 8	7 82	12.1		24 26	20 40 42
Volume at 350°C x Section 1.5	5 %	± + % + + 9	= 4 5	2 7 3 3	. 5 5	2 5 2	- 8	32	34 30	30 40 42
Volume at 350°C			•				1	0.7		
95	Vol	ume at 350°C					,			Kernel Density
94	90 7						*	0.6 -	\wedge	
94	95 +							0.5 -		
91	94 -						_	0.4	/ \	
90 A A A A A A A A A A A A A A A A A A A	93			Δ Δ Δ	Δ Δ Δ	Δ 2		0.4	/ \	
91 0.2 0.1 0.1	92		ΔΔ					0.3 -	/ \	
0.1	Δ -	•						0.2	// \	
	91 +							J.2	// \	
	90 +						—	0.1	/	/ _
· · · · · · · · · · · · · · · · · · ·	h m	02	5 5 24 9 9 94	3.6 66 53	£ 2 4	21 76	- s s		02	
	£ 8	K 9 0 0 90 H 80 88 81 82 82 82 83 83 83 83 83 83 83 83 83 83 83 83 83	9 K A	£ \$ \$ £	627 627	5 2 20 20 20 20 20 20 20 20 20 20 20 20 2	6 33 12	90	92 9	96 98

Determination of FAME on sample #21045; result in %V/V

lab	method	value	mark	z(targ)	remarks
171	D7371	7.63	G(0.01)	4.86	
492					
496	EN14078-B	6.87		0.56	
541					
824					
962					
963	EN14078-A	6.85	С	0.45	first reported 6.2
1121					·
1126	EN14078-A	6.7		-0.40	
1141					
1259	EN14078-A	6.8		0.17	
1320					
1556	EN14078-A	6.6829		-0.49	
1720					
1753					
1776	EN14078-A	6.71		-0.34	
1806					
1854	EN14078-B	6.75		-0.11	
1857	EN14078	6.95		1.02	
1980	EN14078-B	6.82		0.28	
6018	EN14078-B	6.6258		-0.82	
6028	EN14078-B	6.9		0.73	
6075	211110102				
6201	EN14078-A	6.52		-1.41	
6274	EN14078-B	6.96		1.07	
6366	EN14078-A	6.644		-0.71	
6378	2111407071				
0070					
	normality	OK			
	n	14			
	outliers	1			
	mean (n)	6.770			
	st.dev. (n)	0.1303			
	R(calc.)	0.365			
	st.dev.(EN14078-B:14)	0.1770			
	R(EN14078-B:14)	0.496			application range: 3-20 %V/V
	compare	0.430			application range. 5-20 /0 V/ V
	R(EN14078-A:14)	0.361			application range: 0.05-3 %V/V
	N(EN 14070-A. 14)	0.301			application range. 0.05-3 70 V/V





Determination of Flash Point PMcc on sample #21045; result in °C

lab	method	value	mark	z(targ)	remarks
171	D93-A	<40			
492					
496	ISO2719-A	<40			
541	ISO2719-A	<40.0			
824	ISO2719-A	<40.0			
962	D93-A	<40.0			
963	ISO2719-A	<40.0			
1121	ISO2719-A	<40			
1126					
1141	ISO2719-A	< 40			
1259	D93-A	30.0			
1320					
1556	ISO2719-A	<40			
1720					
1753	ISO2719-A	21.5			
1776	ISO2719-A	<40			
1806	ISO2719-A	22			
1854	D93-A	LT 40			
1857	ISO2719	24			
1980	ISO2719-B	<40,0			
6018	ISO2719-A	<40,0 [37,0]			
6028	ISO2719-A	28.0			
6075					
6201	D93-A	22.0			
6274	D93-A	21			
6366	D93-A	<40.0			
6378					
	n	21			
	mean (n)	<40			

Determination of Kinematic Viscosity at 40°C on sample #21045; result in mm²/s

lab	method	value	mark	z(targ)	remarl	ks								
171	D445	2.822		1.00										
492 496 541	ISO3104	 2.7918		 -1.70										
824	ISO3104	2.7910		0.02										
962	D445	2.815	С	0.38	first re	oorted	2.75							
963	ISO3104	2.817		0.56										
1121 1126	ISO3104	2.8074		-0.30 										
1141														
1259 1320	ISO3104	2.788		-2.04 										
1556	ISO3104	2.8059		-0.44										
1720	D7042	2.817		0.56										
1753 1776	ISO3104 D7042	2.8046 2.786		-0.56 -2.22										
1806	ISO3104	2.8029		-0.71										
1854	1000404													
1857 1980	ISO3104 ISO3104	2.8088 2.8221		-0.18 1.01										
6018	ISO3104	2.8503		3.54										
6028	ISO3104	2.827		1.45										
6075 6201	ISO3104 ISO3104	2.772 2.812		-3.48 0.11										
6274	D445	2.843		2.89										
6366	D445	2.8122		0.13										
6378														
	normality	OK												
	n outliers	20 0												
	mean (n)	2.8108												
	st.dev. (n)	0.01828												
	R(calc.) st.dev.(ISO3104:20)	0.0512 0.01116												
	R(ISO3104:20)	0.0312												
2.86 T														
2.84													Δ	
2.82 -							^	Δ	Δ	Δ	Δ	Δ		
2.8	A	Δ Δ	Δ Δ	Δ Δ	Δ		-							
2.78	Δ Δ Δ													
2.76														
2.74														
2.72														
6075	1259	1806	1556	1857	6201	9989	3962	963	1720	171	1980	6028	6274	6018
35														
		Kernel	Density											
30	1	^												
		$/ \setminus$												
25	1	/ \												
20	=													
15		// \												
15		// \\												
10	1	<i>!</i> \												
	/	\\												
5	1 /	V												
0				_										
2	2.7 2.75	2.8 2	.85	2.9										

Determination of Lubricity by HFRR at 60°C on sample #21045; result in μm

lab	method	value	mark	z(targ)	Corrected	remarks	
171	D6079	202		0.68			
492 496	ISO12156-1-A	 187		0.16	 No		
541							
824 962	ISO12156-1-A	173		-0.33 	Yes 		
963	ISO12156-1 (2006)	185		0.09	Yes		
1121 1126							
1141							
1259	ISO12156-1-A	180		-0.09	 NI		
1320 1556	ISO12156-1-A ISO12156-1-A	190 159		0.26 -0.82	No No		
1720							
1753 1776							
1806	10040450 4 4	400			 V		
1854 1857	ISO12156-1-A ISO12156-1-B	183 177		0.02 -0.19	Yes No		
1980							
6018 6028	ISO12156-1-A	 175		-0.26			
6075	ISO12156-1-A	211		1.00	No		
6201 6274	ISO12156-1-A ISO12156-1-A	160 160	С	-0.79 -0.79	No Yes	first reported 260	
6366	ISO12156-1-A	212.8		1.06	Yes		
6378							
	normality	OK					
	n outliers	14 0					
	mean (n)	182.486					
	st.dev. (n) R(calc.)	17.4121 48.754					
	st.dev.(ISO12156-1-A:18)	28.5714					
	R(ISO12156-1-A:18) compare	80	(digital ca	mera)			
	R(ISO12156-1-B:18)	90	(1	visual)			
	R(D6079:18)	80					
300 T							
250 -							
200 -					Δ Δ	Δ Δ	Δ
450	Δ Δ Δ	Δ	Δ	Δ Δ			
150 -							
100 -							
50							
20	6201	6028	1259	1854	496	171	9366
0.025							
0.025	12	(ernel Density					
	<u></u>	Cerrier Delisity					
0.02 -	-						
0.015 -							
0.010							
0.01 -	-	V					
		\\					
0.005 -	<u> </u>	\\					
0.000		\\					
	<i>f</i>	//					
0 -	0 100	200 30	00				
'	0 100	200 30	~				

Determination of Manganese as Mn on sample #21045; result in mg/L

lab	method	value	mark	z(targ)	remarks
171	D3831	<0.25			
492					
496	EN16576	<0.5			
541					
824					
962					
963					
1121					
1126					
1141					
1259					
1320					
1556					
1720					
1753					
1776					
1806					
1854					
1857	EN16576	0.01			
1980	EN16576	<0,50			
6018					
6028	EN16576	0.15			
6075					
6201	EN16576	0.01			
6274	EN16576	<0.5			
6366					
6378					
	n	7			
	mean (n)	<0.5			application range: 0.5 - 7 mg//L
					-

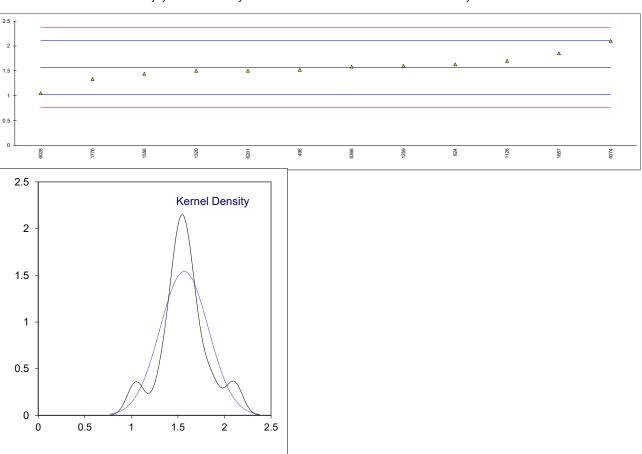
Determination of Nitrogen on sample #21045; result in mg/kg

lab	method	value	mark	z(targ)	remarks					
171	D4629	14	G(0.05)	-4.54						
492										
496 541										
824	D4629	20.6		0.32						
962	D4629	20.8		0.47						
963 1121	D4629	21.3		0.83						
1126										
1141										
1259	D.4000	40.0								
1320 1556	D4629 D4629	19.9 18.72		-0.20 -1.07						
1720	D4629	20.12		-0.03						
1753										
1776 1806	D4629	19.6 		-0.42						
1854										
1857	D4629	20.3		0.10						
1980										
6018 6028										
6075										
6201	D4629	23.12	DG(0.05)	2.17						
6274	D4000		DC(0.05)	2.07						
6366 6378	D4629	24.2	DG(0.05)	2.97						
00.0										
	normality	OK								
	n outliers	8 3								
	mean (n)	20.17								
	st.dev. (n)	0.791								
	R(calc.) st.dev.(D4629:17)	2.21 1.358								
	St. dev.(D4029.17)	1.330								
	R(D4629:17)	3.80								
00	R(D4629:17)	3.80								
30 T	R(D4629:17)	3.80								
30 7	R(D4629:17)	3.80							*	ж
	R(D4629:17)	3.80	Δ	Δ	Δ.	Δ	Δ	Δ	×	*
25 -	R(D4629:17)	3.80	Δ	Δ	Δ	^	Δ	Δ	×	x
25 -	R(D4629:17)	3.80	Δ	Δ	۵	Δ	Δ	Δ	×	*
25 -	R(D4629:17)	3.80	Δ	Δ	•	Δ	Δ	Δ	×	x
25 20 15 10	R(D4629:17)	3.80	Δ	Δ	Δ	Δ	Δ	Δ	×	x
25 - 20 - 15 -	R(D4629:17)	3.80	Δ	Δ	Δ	Δ	Δ	Δ	×	*
25 20 15 10 5	R(D4629:17) Δ x	3.80	4 020	4	- ▲	100	Δ			*
25 20 15 10 5	R(D4629:17)	3.80	0261	4200	1857	A 778	A 226	Δ 28 8	¥	**************************************
25 - 20 - 15 - 10 - 5 -	R(D4629:17) Δ x	3.80	Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q	0.00 T	△	824	A 206			
25 20 15 10 5	R(D4629:17) Δ x	3.80		4720	1957	A 900	A 286			X
25 - 20 - 15 - 10 - 5 - 0	R(D4629:17) Δ x	3.80 <u>A</u>	® Republic Property	4720	4	A 162	2206			* * * * * * * * * * * * * * * * * * *
25 - 20 - 15 - 10 - 5 -	R(D4629:17) Δ x	3.80 <u>A</u>		1720	4	A 728	2206			**
25 - 20 - 15 - 10 - 5 - 0	R(D4629:17) Δ x	3.80 <u>A</u>		1720	1857	824	226			**************************************
25 - 20 - 15 - 10 - 5 - 0	R(D4629:17) Δ x	3.80 <u>A</u>		1720	4 4/581	929	A 2006			**************************************
25 - 20 - 15 - 10 - 5 - 0 0.6 - 7 0.5 -	R(D4629:17) Δ x	3.80 <u>A</u>		4720	1657	1728	200			**************************************
0.6 ¬ 0.5 ¬ 0.4 ¬	R(D4629:17) Δ x	3.80 <u>A</u>		4.720	1957	W28	A 286			
25 - 20 - 15 - 10 - 5 - 0 0.6 - 7 0.5 -	R(D4629:17) Δ x	3.80 <u>A</u>		1720	4	824	786			
0.6 ¬ 0.5 ¬ 0.4 ¬	R(D4629:17) Δ x	3.80 <u>A</u>		02211	4	A 1702	2206			
0.6 ¬ 0.5 ¬ 0.4 ¬ 0.3 ¬	R(D4629:17) Δ x	3.80 <u>A</u>		0221	4	A 1728	2206			**
0.6 ¬ 0.5 ¬ 0.4 ¬	R(D4629:17) Δ x	3.80 <u>A</u>		1720	1867	A 778	2246			**************************************
0.6 - 0.5 - 0.3 - 0.2 -	R(D4629:17) Δ x	3.80 <u>A</u>		1720	4	824	Δ			***************************************
0.6 ¬ 0.5 ¬ 0.4 ¬ 0.3 ¬	R(D4629:17) Δ x	3.80 <u>A</u>		4720	4.2591	82%	∆			**************************************
0.6 - 0.5 - 0.3 - 0.2 -	R(D4629:17) Δ x	3.80 <u>A</u>		41720	1957	N28	A 280			**************************************
0.6 - 0.5 - 0.4 - 0.2 - 0.1 -	R(D4629:17) Δ x	3.80 Kern	nel Density		1857	A 100	206			
0.6 - 0.5 - 0.4 - 0.2 - 0.1 -	R(D4629:17) Δ x	3.80 <u>A</u>	nel Density	30	4	A 728	2296			

Determination of Polycyclic Aromatic Hydrocarbons ¹⁾ on sample #21045; result in %M/M

lab	method	value	mark	z(targ)	remarks
171					
492					
496	EN12916	1.52		-0.18	
541					
824	EN12916	1.63		0.23	
962					
963 1121					
1121	EN12916	1.7		0.49	
1141	EN12910	1.7		0.49	
1259	EN12916	1.6	С	0.12	first reported 2.0
1320	EN12916	1.50	O	-0.25	mot reported 2.0
1556	EN12916	1.44		-0.47	
1720					
1753					
1776	EN12916	1.333		-0.87	
1806					
1854					
1857	EN12916	1.85		1.05	
1980					
6018	EN140040	4.05		4.00	
6028 6075	EN12916	1.05		-1.92 	
6201	EN12916	1.5		-0.25	
6274	EN12916	2.1		1.98	
6366	EN12916	1.585		0.07	
6378					
	normality	suspect			
	n	12			
	outliers	0			
	mean (n)	1.567			
	st.dev. (n)	0.2588			
	R(calc.)	0.725			
	st.dev.(EN12916:16) R(EN12916:16)	0.2696 0.755			
	11(112310.10)	0.700			

¹⁾Definition from EN12916: %Polycyclic Aromatic Hydrocarbons = sum of %di and %tri+ Aromatic Hydrocarbons



Determination of Mono Aromatic Hydrocarbons on sample #21045; result in %M/M

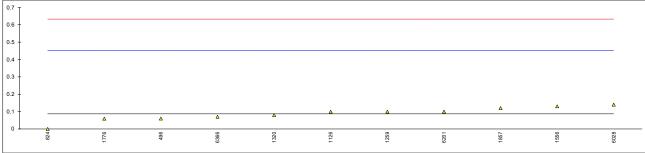
lab	method	value	mark	z(targ)	remarks				
171									
492 496	EN12916	 15.07		-0.35					
541									
824	EN12916	14.96		-0.51					
962 963									
1121									
1126 1141	EN12916	15.0 		-0.45					
1259	EN12916	15.9	С	0.90	first reported	17.7			
1320	EN12916	15.07		-0.35	·				
1556 1720	EN12916	16.120 		1.23					
1753									
1776	EN12916	14.88824		-0.62					
1806 1854									
1857	EN12916	16.13		1.25					
1980 6018									
6028									
6075									
6201 6274	EN12916 EN12916	14.9 		-0.60 					
6366	EN12916	14.965		-0.50					
6378									
	normality	suspect							
	n	10							
	outliers mean (n)	0 15.300							
	st.dev. (n)	0.5243							
	R(calc.)	1.468							
	st.dev.(EN12916:16) R(EN12916:16)	0.6640 1.859							
18 T									
17									
16.5 -	·							Δ	Δ
15.5							Δ		
15 -	Δ Δ	Δ	Δ	Δ	Δ	Δ			
14.5									
13.5 -									
13	6201	824	9900	1126	96	1320	1259	1556	1857
1 -				7					
0.9	-	∧ Kernel	Density						
0.8 -		/ \							
		l h							
0.7	1	/ // \							
0.6	_	′ /							
0.5		/ \ \							
]	/							
0.4	1								
0.3		\ \ \ \							
		$\vee \setminus \setminus$							
0.2	1	\ \							
0.1 -	1 //	\	\						
0 -	<u> </u>			_					
1	12 14	16		18					

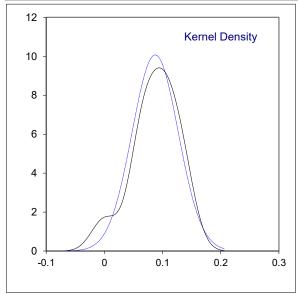
Determination of Di Aromatic Hydrocarbons on sample #21045; result in %M/M

lab	method	value	mark	z(targ)	remarks				
171									
492 496	EN12916	 1.46		 -0.15					
541									
824 962	EN12916	1.63		0.90					
962 963									
1121									
1126 1141	EN12916	1.6 		0.72					
1259	EN12916	1.5	С	0.10	first reported 1.8				
1320 1556	EN12916 EN12916	1.42 1.3115		-0.40 -1.07					
1720	21112010								
1753 1776	EN12916	 1.27401		-1.30					
1806	LIV12910			-1.50					
1854	EN40040	4.70		4.50					
1857 1980	EN12916	1.73 		1.52					
6018	EN40040		0(0.05)						
6028 6075	EN12916	0.91	G(0.05)	-3.56 					
6201	EN12916	1.4		-0.52					
6274 6366	EN12916	 1.515		0.19					
6378	- · -								
	normality	OK							
	n	10							
	outliers mean (n)	1 1.484							
	st.dev. (n)	0.1422							
	R(calc.) st.dev.(EN12916:16)	0.398 0.1613							
	R(EN12916:16)	0.452							
2.1 T									
1.9									
1.7							Δ	Δ	Δ
1.5		Δ	. Δ		Δ Δ	Δ			
1.1	Δ								
0.9	ж								
0.7									
0.5	1776	1556	1320		1259	9989	1126	824	1857
3 -		44 11	D 11						
		Kernel	Density						
2.5 -									
2 -	1								
		/ \							
1.5 -	-	/ \							
1 -	-								
		// \							
0.5 -	-	// \\							
		/ \/	\						
0 -			<u> </u>						
1 (0 0.5 1	1.5	2 2.	5					

Determination of Tri⁺ Aromatic Hydrocarbons on sample #21045; result in %M/M

lab	method	value	mark	z(targ)	remarks
171					
492					
496	EN12916	0.06		-0.15	
541	EN140040				
824	EN12916	0		-0.48	
962					
963 1121					
1121	EN12916	0.1		0.07	
1141	ENIZSIO	U. I			
1259	EN12916	0.1	С	0.07	first reported 0.2
1320	EN12916	0.08	J	-0.04	mot reported 0.2
1556	EN12916	0.1302		0.24	
1720					
1753					
1776	EN12916	0.0589923		-0.16	
1806					
1854					
1857	EN12916	0.12		0.18	
1980					
6018	EN140040				
6028	EN12916	0.14		0.29	
6075 6201	EN12916	0.1		0.07	
6274	EN12910	0.1		0.07	
6366	EN12916	0.07		-0.09	
6378	LIVI2510			-0.00	
0010					
	normality	suspect			
	n	11			
	outliers	0			
	mean (n)	0.087			
	st.dev. (n)	0.0396			
	R(calc.)	0.111			
	st.dev.(EN12916:16)	0.1820			
	R(EN12916:16)	0.510			
0.7 -					





Determination of Total Aromatic Hydrocarbons on sample #21045; result in %M/M

lab	method	value	mark	z(targ)	remarks				
171 492									
496	EN12916	16.59		-0.43					
541 824	EN12916	16.59		-0.43					
962 963									
1121	- 1110010								
1126 1141	EN12916	16.7 		-0.26 					
1259 1320	EN12916 EN12916	17.5 16.57	С	0.98 -0.46	first reported	19.5			
1556	EN12916	17.562		1.08					
1720 1753									
1776 1806	EN12916	16.22124 		-1.00 					
1854 1857	EN12916	 17.98		1.73					
1980	LIV12910			1.73					
6018 6028									
6075 6201	EN12916	 16.4		 -0.72					
6274	EN12916								
6366 6378	EN12916	16.55 		-0.49 					
	normality	suspect							
	n	10							
	outliers mean (n)	0 16.866							
	st.dev. (n) R(calc.)	0.5895 1.651							
	st.dev.(EN12916:16) R(EN12916:16)	0.6454 1.807							
	1 (21112010.10)								
20 T									
18 -									Δ
17 -		Δ	Δ	<u> </u>	Δ	Δ	Δ	Δ	
16 -	Δ Δ								
15 -									
13									
	6201	9999	1320		824	1126	1259	1556	1857
0.9				7					
0.8	-	Kernel	Density						
0.7] /	1							
		h							
0.6	-	$/ \setminus \setminus$							
0.5	-								
0.4	-								
0.3 -]								
		\sim \setminus							
0.2	/	//							
0.1 -	1 /	//							
0 -	<u> </u>	47	10						
1	13 15	17 1	9	21					

Determination of Pour Point Manual on sample #21045; result in °C

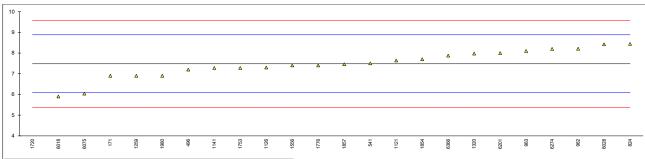
lab	method	value	mark	z(targ)	remarks							
171	D97	-33		-0.27								
492	10.000 10											
406	ISO3016-	22		0.07								
496 541	automated	-33 		-0.27 								
824	ISO3016-manual	-33		-0.27								
962	D97	-33		-0.27								
963	ISO3016-manual	-33		-0.27								
121	ISO3016-manual	< -24										
126												
141	ISO3016-manual	-33		-0.27								
259	ISO3016-manual	-33		-0.27								
320	ISO3016-manual ISO3016-	-30		0.66								
556 720	automated	-30 		0.66								
753	D97	-30		0.66								
776	B07											
806	D97	-30		0.66								
854 857	ISO3016-manual ISO3016-manual	-33 -30		-0.27 0.66								
	ISO3016-											
980	automated	-30	0(0.05)	0.66								
018	ISO3016-manual	-39	G(0.05)	-2.14								
028 075												
201	ISO3016-manual	-36		-1.21								
274	ISO3016-	22		0.27								
366	automated D97	-33 -33		-0.27 -0.27								
378	Dar			-0.27								
	normality	OK										
	n	17										
		1										
	n outliers mean (n)	1 -32.12										
	n outliers mean (n) st.dev. (n)	1 -32.12 1.764										
	n outliers mean (n) st.dev. (n) R(calc.)	1 -32.12 1.764 4.94										
	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:1	1 -32.12 1.764 4.94 9) 3.214										
	n outliers mean (n) st.dev. (n) R(calc.)	1 -32.12 1.764 4.94										
т	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:1	1 -32.12 1.764 4.94 9) 3.214										
T _	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:1	1 -32.12 1.764 4.94 9) 3.214										
_	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:1	1 -32.12 1.764 4.94 9) 3.214										
_ -	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:1	1 -32.12 1.764 4.94 9) 3.214										
<u> </u>	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:1	1 -32.12 1.764 4.94 9) 3.214					Δ	Δ	Δ	Δ	Δ	Δ
- - -	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:1 R(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214	Δ Δ	Δ Δ	Δ Δ	Δ	Δ	Δ	Δ	Δ	Δ	Δ
- - -	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:1 R(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	Δ Δ	Δ Δ	Δ Δ	Δ	Δ	Δ	Δ	Δ	Δ	Δ
·	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	Δ Δ	Δ Δ	Δ Δ	Δ	Δ	Δ	Δ	Δ	Δ	Δ
- - -	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	Δ Δ	Δ Δ	Δ Δ	Δ	Δ	Δ	Δ	Δ	Δ	Δ
× - ×	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9		A 4								
* × - 81.09	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9		1141 1250 2002	A 4 17.29	△	Δ (25)	△	Δ	Δ	■ 1588	△
× ×	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1259 P								
× × ×	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9		1259								
	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1441 1289 a								
.25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1141								
.25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1141 1020 1020								
.25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1441 2008								
).25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1411 Title 1 T								
).25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1141								
).25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	T 141								
).25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4								
0.25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1141 T 1289 A								
0.25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1741								
0.2 -	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1230								
).25 · · · · · · · · · · · · · · · · · · ·	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1259								
0.25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5								
2.25 0.25 0.15	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	4141								
).25 · · · · · · · · · · · · · · · · · · ·	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	1741								
0.25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	88 89 86 89	7289								
0.25	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	g g Kernel Density									
0.2 - 0.1 - 0	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	g g Kernel Density	-20								
0.2 · 0.1 · 0.1 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 ·	n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3016:19)	1 -32.12 1.764 4.94 9) 3.214 9	g g Kernel Density									

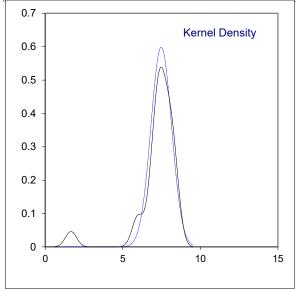
Determination of Pour Point Automated, 3°C interval on sample #21045; result in °C

lab	method	value	mark	z(targ)	remarks			
171	D5950	-33		-0.86				
492								
496	D6892	-33		-0.86				
541	D5950	-30		0.52				
824 962								
963	D5950	-33		-0.86				
1121	D0000			-0.00				
1126								
1141								
1259								
1320								
1556 1720								
1753								
1776	D5950	-30		0.52				
1806								
1854								
1857 1980								
6018								
6028	D5950	-30		0.52				
6075	NF T60-105	-30		0.52				
6201	D5950	-30		0.52				
6274								
6366 6378								
0370								
	normality	unknown						
	n	8						
	outliers	0						
	mean (n) st.dev. (n)	-31.13 1.553						
	R(calc.)	4.35						
	st.dev.(D5950:14)	2.179						
	R(D5950:14)	6.1						
-20 T								
-25 -								
-30	Δ Δ		Δ	Δ	Δ	Δ	Δ	
-35	Δ Δ	<u> </u>	Δ					
	-							
-40 +								
-45								
	171	26	963	22	1776	6028	6075	6201
2.0								
0.3				\neg				
		∧ Kerr	nel Density					
0.25	_	\wedge /\						
		/						
		/ /\ \						
0.2	1	/ / \ \						
0.15	\downarrow	/ \\						
0.15	//	_ / \\						
	1 // '	\						
0.1	4 //	<u> </u>						
		\\						
] //	1						
0.05	1 //	/						
	//	/						
0								
"-	40 -35	-30	-25	-20				
1								

Determination of Sulfur on sample #21045; result in mg/kg

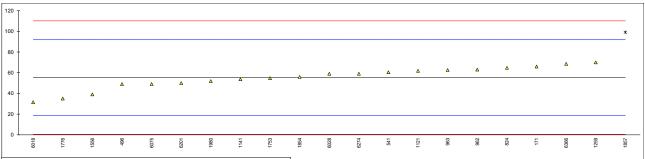
lab	method	value	mark	z(targ)	remarks
171	D5453	6.9		-0.83	
492					
496	ISO20846	7.2		-0.40	
541	ISO20846	7.50		0.03	
824	D5453	8.44		1.37	
962	D5453	8.21		1.05	
963	ISO20846	8.1		0.89	
1121	D5453	7.64		0.23	
1126	ISO20846	7.3		-0.26	
1141	ISO20846	7.28		-0.28	
1259	ISO20846	6.9		-0.83	
1320	ISO20846	7.97		0.70	
1556	ISO20884	7.4		-0.11	
1720	D5453	1.66	R(0.01)	-8.32	
1753	ISO20846	7.28		-0.28	
1776	ISO20846	7.4		-0.11	
1806					
1854	ISO20846	7.7		0.32	
1857	ISO20846	7.46		-0.03	
1980	ISO20884	6.90		-0.83	
6018	ISO20846	5.9		-2.26	
6028	ISO20846	8.42		1.35	
6075	ISO20846	6.04		-2.06	
6201	ISO20846	8		0.75	
6274	ISO20846	8.2		1.03	
6366	D5453	7.875		0.57	
6378					
	normality	OK			
	n	23			
	outliers	1			
	mean (n)	7.479			
	st.dev. (n)	0.6662			
	R(calc.)	1.865			
	st.dev.(ISO20846:19)	0.6992			
	R(ISO20846:19)	1.958			

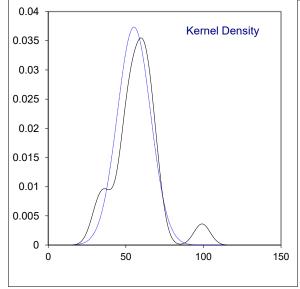




Determination of Water on sample #21045; result in mg/kg

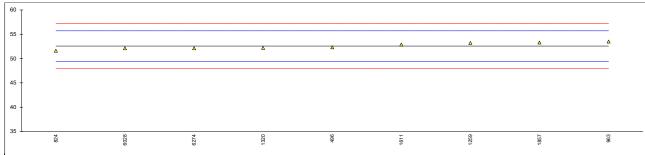
lab	method	value	mark	z(targ)	remarks
171	D6304-A	66		0.59	
492					
496	ISO12937	49		-0.34	
541	ISO12937	60.5		0.29	
824	ISO12937	64.7		0.52	
962	D6304-A	63		0.42	
963	ISO12937	62.685		0.41	
1121	ISO12937	61.8		0.36	
1126					
1141	ISO12937	53.726		-0.08	
1259	ISO12937	70		0.81	
1320					
1556	ISO12937	39		-0.89	
1720					
1753	ISO12937	54.7		-0.03	
1776	ISO12937	35		-1.11	
1806					
1854	D6304-C	56		0.04	
1857	ISO12937	99.1	R(0.05)	2.40	
1980	ISO12937	52		-0.18	
6018	ISO12937	31.55		-1.30	
6028	ISO12937	59		0.20	
6075	ISO12937	49.1		-0.34	
6201	ISO12937	50		-0.29	
6274	ISO12937	59		0.20	
6366	D6304-A	68.55		0.73	
6378					
		011			
	normality	OK			
	n	20			
	outliers	1			
	mean (n)	55.27			
	st.dev. (n)	10.680			
	R(calc.)	29.90			
	st.dev.(ISO12937:00)	18.259			
	R(ISO12937:00)	51.12			
120 T					
-					
100					

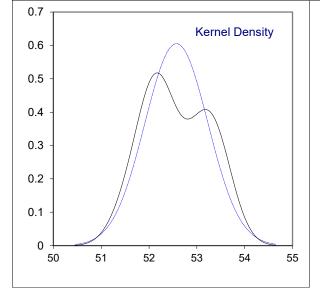




Determination of Cetane Number on sample #21046;

lab	method	value	mark	z(targ)	remarks
496	ISO5165	52.3		-0.18	
824	D613	51.6		-0.62	
963	ISO5165	53.5		0.59	
1259	ISO5165	53.2		0.40	
1320	ISO5165	52.2		-0.24	
1556					
1611	ISO5165	52.87		0.19	
1644					
1713					
1776					
1857	ISO5165	53.3		0.46	
6028	ISO5165	52.1		-0.30	
6075					
6274	ISO5165	52.1		-0.30	
	normality	OK			
	n	9			
	outliers	0			
	mean (n)	52.57			
	st.dev. (n)	0.659			
	R(calc.)	1.846			
	st.dev.(ISO5165:20)	1.56			
	R(ISO5165:20)	4.37			
60 T					





Determination of Derived Cetane Number (EN17155) on sample #21046;

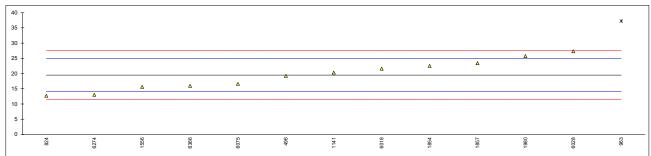
lab	method	DCN	mark	z(targ)	ID (ms)	mark	z(targ)	Air Temp. (°C)	mark
496									
824									
963									
1259									
1320									
1556									
1611									
1644									
1713									
1776									
1857									
6028									
6075	EN17155	52.28			2.2847			579.57	
6274									

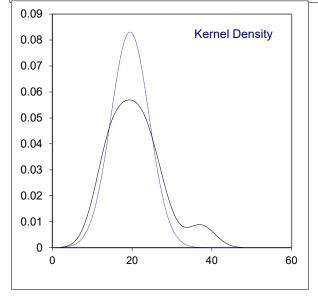
Determination of Derived Cetane Number (EN16715) on sample #21046;

lab method	DCN mark	z(targ) ID (ms) mark	z(targ) CD (ms) mark	z(targ) W. T. (°C)
496 EN16715	52.2	-2.16 3.04	0.33 4.535	1.72
824				
963				
1259 1320				
1556 EN16715	54.75	2.61 2.97	-0.92 4.35	-2.33 583.21
1611				
1644 EN16715	53.00	-0.66 3.0309	0.16 4.4866	0.66 599.75
1713 EN16715 1776 EN16715	53.20 53.62	-0.29 3.0275 0.50 3.04	0.10 4.4701 0.33 4.44	0.30 586.77 -0.36 589.22
1857	55.02	0.50 3.04	0.33 4.44	-0.30 369.22
6028				
6075				
6274			 I	 I
normality	unknown	unknown	unknown	
n	5	5	5	
outliers	0	0	0	
mean (n) st.dev. (n)	53.35 0.935	3.02 0.029	4.46 0.069	
R(calc.)	2.62	0.023	0.003	
st.dev.(EN16715	i:15) 0.535	0.056	0.05	
R(EN16715:15)	1.50	0.16	0.13	
56 т				
DCN				
55 -				Δ
54 -			Δ	
53 -	Δ	Δ		
52 +				
<u> </u>				
51 +				
50	1644	1713	1776	1556
4		11		45
3.25				
3.15 - ID				
3.05 +	•	٨	A	Δ
2.95 +				
2.85				
2.75 -				
2.65				
2.55	1713	1644	964	1776
				-
4.7				
4.6 - CD				
4.5 -			Δ	Δ
4.4 +	Δ	Δ		
4.3				
4.2				
4.1 +				
4 1 959	1776	1713	1644	496
-	÷	÷	-	

Determination of Total Contamination on sample #21047; result in mg/kg

lab	method	Total C.	mark	z(targ)	incomplete	vol. filtered (mL)	stopped (min)	remarks
496	EN12662:2008	19.21		-0.11	Yes			
824	EN12662:2014	12.7		-2.52		300		
963	EN12662:2014	37.23	C,G(0.05)	6.59	Yes	300	5	first reported 4.14
1141	EN12662:2014	20.3		0.30	Yes	300		
1320								
1556	EN12662:2014	15.61		-1.44	Yes	300	1	
1854	EN12662:2014	22.5	С	1.12	No	300		first reported 35.5
1857	EN12662	23.4		1.45	Yes	300		
1980	EN12662:2014	25.74		2.32	Yes	251.2		
6018	EN12662:2014	21.6		0.78				
6028	EN12662:2014	27.3		2.90				
6075	EN12662:2014	16.6		-1.07	Yes			
6274	EN12662:2014	13		-2.41	Yes	300		
6366	EN12662:2014	15.96		-1.31	Yes	300	1	
	normality	OK						
	n	12						
	outliers	1						
	mean (n)	19.493						
	st.dev. (n)	4.8023						
	R(calc.)	13.446						
	st.dev.(EN12662:14)	2.6929						
	R(EN12662:14)	7.540						





APPENDIX 2

Number of participants per country

- 1 lab in ARGENTINA
- 1 lab in CROATIA
- 2 labs in GERMANY
- 1 lab in GREECE
- 1 lab in MALYSIA
- 1 lab in MARTINIQUE
- 2 labs in NETHERLANDS
- 4 labs in POLAND
- 1 lab in POTRUGAL
- 2 labs in ROMANIA
- 1 lab in RUSSIAN FEDERATION
- 2 labs in SAUDI ARABIA
- 1 lab in SERBIA
- 1 lab in SLOVAKIA
- 1 lab in SOUTH KOREA
- 1 lab in SUDAN
- 2 labs in SWEDEN
- 1 lab in TUNISIA
- 1 lab in TURKEY
- 1 lab in UGANDA
- 1 lab in UNITED KINGDOM
- 1 lab in UNITED STATES OF AMERICA

APPENDIX 3

Abbreviations

C = final test result after checking of first reported suspect test result

D(0.01) = outlier in Dixon's outlier test
D(0.05) = straggler in Dixon's outlier test
G(0.01) = outlier in Grubbs' outlier test
G(0.05) = straggler in Grubbs' outlier test
DG(0.01) = outlier in Double Grubbs' outlier test
DG(0.05) = straggler in Double Grubbs' outlier test

R(0.01)/R(1) = outlier in Rosner's outlier test R(0.05)/R(5) = straggler in Rosner's outlier test

E = calculation difference between reported test result and result calculated by iis

W = test result withdrawn on request of participant ex = test result excluded from statistical evaluation

n.a. = not applicable
n.e. = not evaluated
n.d. = not detected
fr. = first reported

f+? = possibly a false positive test result? f-? = possibly a false negative test result?

SDS = Safety Data Sheet

Literature

- 1 iis Interlaboratory Studies, Protocol for the Organisation, Statistics & Evaluation, June 2018
- 2 ISO5725:86
- 3 ISO5725 parts 1-6:94
- 4 ISO13528:05
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- 6 W.J. Youden and E.H. Steiner, Statistical Manual of the AOAC, (1975)
- 7 P.L. Davies, Fr. Z. Anal. Chem, <u>331</u>, 513, (1988)
- 8 J.N. Miller, Analyst, <u>118</u>, 455, (1993)
- 9 Analytical Methods Committee, Technical Brief, No 4, January 2001
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- 11 W. Horwitz and R. Albert, J. AOAC Int, <u>79, 3</u>, 589-621, (1996)
- Bernard Rosner, Percentage Points for a Generalized ESD Many-Outlier Procedure, Technometrics, 25(2), 165-172, (1983)